15-830 – Control 3: Control of Dynamical Systems

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PID Control

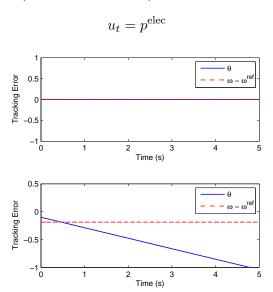
- Proportional Integral Derivative
- Remember linear system of generator

$$\dot{\theta} = \omega - \omega^{\text{ref}}$$

$$\dot{\omega} = \frac{1}{2H}(u - p^{\text{elec}})$$

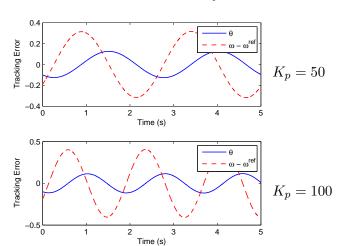
• Goal is to achieve/maintain $\theta = 0$

• Attempt #1 (feed-forward control):



• Attempt #2 (P control):

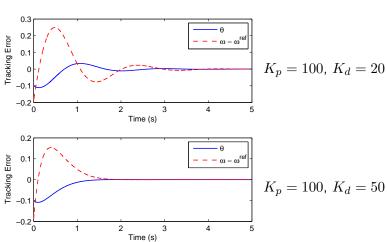
$$u_t = p^{\text{elec}} + K_p(\theta_t^d - \theta_t)$$
$$= p^{\text{elec}} - K_p\theta_t$$



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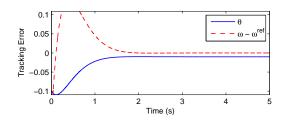
• Attempt #2 (PD Control):

$$u_t = p^{\text{elec}} + K_p(\theta_t^d - \theta_t) + K_d(\dot{\theta_t}^d - \dot{\theta_t})$$
$$= p^{\text{elec}} - K_p\theta_t - K_d(\omega_t - \omega^{\text{ref}})$$



ullet Looks good, but what if we don't know $p^{
m elec}$ beforehand?

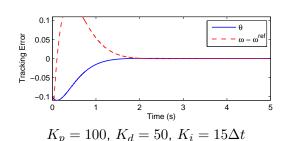
$$u_t = K_p(\theta_t^d - \theta_t) + K_d(\dot{\theta_t}^d - \dot{\theta_t})$$



ullet θ never reaches desired value

• Attempt #3 (PID Control):

$$u_t = K_p(\theta_t^d - \theta_t) + K_d(\dot{\theta}_t^d - \dot{\theta}_t) + K_i \sum_{\tau=1}^t (\theta_\tau^d - \theta_\tau)$$
$$= -K_p\theta_t - K_d(\omega_t - \omega^{\text{ref}}) - K_i \sum_{\tau=1}^t \theta_\tau$$



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Multi-variate PID control

- PID control works well for controlling "single input, single output" (SISO) systems
 - For second order linear systems, it is the "optimal" method
- For higher-order or multi-variate systems, it is no longer optimal, but often works well anyway
- Can require a fair amount of tuning

Example: multiple generators and DC power flow approximation

$$\begin{vmatrix} \dot{\theta}_i = \omega_i - \omega^{\text{ref}} \\ \dot{\omega}_i = \frac{1}{2H_i} (u_i - p_i) \end{vmatrix} i \in \text{GEN}$$

$$p = B\theta$$

 A set of differential algebraic equations, but since algebraic equations are linear, we can invert them directly to form ordinary differential equations

$$\left[\begin{array}{c} p_G \\ p_L \end{array}\right] = \left[\begin{array}{cc} B_{GG} & B_{GL} \\ B_{LG} & B_{LL} \end{array}\right] \left[\begin{array}{c} \theta_G \\ \theta_L \end{array}\right]$$

• Eliminate θ_L variables

$$p_{L} = B_{LG}\theta_{G} + B_{LL}\theta_{L} \implies \theta_{L} = B_{LL}^{-1}p_{L} - B_{LL}^{-1}B_{LG}\theta_{G}$$
$$p_{G} = B_{GG}\theta_{G} + B_{GL}\theta_{L} = (B_{GG} - B_{GL}B_{LL}^{-1}B_{LG})\theta_{G} + B_{GL}B_{LL}^{-1}p_{L}$$

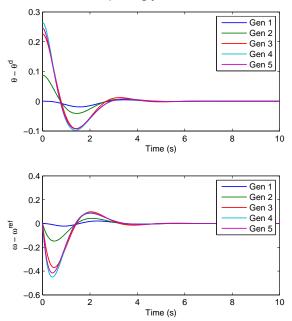
Results in dynamical system

$$\dot{\theta} = \omega - \omega^{\text{ref}}$$

$$\dot{\omega} = \frac{1}{2H} (u - (B_{GG} - B_{GL} B_{LL}^{-1} B_{LG}) \theta - B_{GL} B_{LL}^{-1} p_L)$$

 ω time derivative couples together the dynamics of the different generators

• PID control still works surprisingly well



Linear Quadratic Control

Returning to optimal control formulation

pick
$$u_{1:T}$$
 to minimize $J = \sum_{t=1}^{H} C(x_t, u_t)$

- Remember from intro lecture that we can solve this when dynamics are linear and costs/constraints are convex
- An important special case: linear dynamics and quadratic costs, with no control or state constraints: Linear Quadratic Regulator (LQR)

$$x_{t+1} = Ax_t + Bu_t$$
$$C(x_t, u_t) = ||Qx_t||_2^2 + ||Ru_t||_2^2$$

Can write as the optimization problem

minimize
$$\sum_{x_{1:T}, u_{1:T}}^{H} (\|Qx_t\|_2^2 + \|Ru_t\|_2^2)$$

subject to $x_{t+1} = Ax_t + Bu_t$

 However, it turns out for this special case we get an analytical solution of the form

$$u_t^\star = K_t x_t$$
 for some matrices $K_t \in \mathbb{R}^{m imes n}, \ t = 1, \dots, H$

Derivation is a bit involved, but just linear algebra operations

• Even more interesting: we can solve the *infinite time* problem

minimize
$$\sum_{x_{1:T}, u_{1:T}}^{\infty} \left(\|Qx_t\|_2^2 + \|Ru_t\|_2^2 \right)$$

subject to $x_{t+1} = Ax_t + Bu_t$

and solution is given by steady-state matrix

$$u_t = Kx_t$$

- Intuition: once we achieve $x_t = 0$, $u_{t'} = 0$ and $x_{t'} = 0$ for all $t' \geq t$; if system is controllable, we can achieve this in finite time, so infinite horizon cost is finite
- So common, there is a MATLAB routine for this

• Example: generator control

$$\dot{\theta} = \omega - \omega^{\text{ref}}
\dot{\omega} = \frac{1}{2H} (u - (B_{GG} - B_{GL} B_{LL}^{-1} B_{LG}) \theta - B_{GL} B_{LL}^{-1} p_L)$$

• Write as linear systems

$$\dot{x} = Ax + Bu + a$$

$$x = \begin{bmatrix} \theta \\ \omega \end{bmatrix}$$

$$A = \begin{bmatrix} 0 & I \\ -\frac{1}{2H}(B_{GG} - B_{GL}B_{LL}^{-1}B_{LG}) & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ \frac{1}{2H}I \end{bmatrix}$$

$$a = \begin{bmatrix} -\omega^{\text{ref}}1 \\ -\frac{1}{2H}B_{GL}B_{LL}^{-1}p_L \end{bmatrix}$$

Convert to discrete-time system

$$x_{t+1} = (I + \Delta t A)x_t + \Delta t Bx + \Delta t a$$
$$= \tilde{A}x_t + \tilde{B}x_t + a_t$$

• Given some equilibrium point x^* , u^*

$$x^* = \tilde{A}x^* + Bu^* + a$$

we can convert this affine system to a linear system in the variables $\Delta x_t = x_t - x^*$, $\Delta u_t = u_t - u^*$

$$\Delta x_t = \tilde{A}\Delta x_t + \tilde{B}\Delta u_t$$

Define a cost function on deviation from optimal state

$$C(x_t, u_t) = \|Q(x_t - x^*)\|_2^2 + \|R(u_t - u^*)\|_2^2 = \|Q\Delta x_t\|_2^2 + \|R\Delta u_t\|_2^2$$

• Then optimal LQR solution given by

$$\Delta u_t = K \Delta x_t \Leftrightarrow u_t = u^* + K(x_t - x^*)$$

Notice that the LQR solution

$$u_t = u^* + K(x_t - x^*)$$

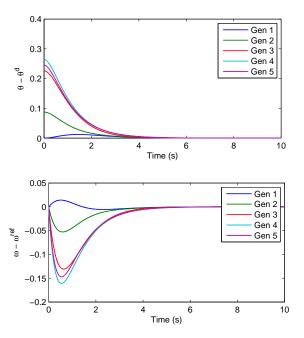
is a generalization of the PD controller with feedforward control

$$u_t = u^* + \begin{bmatrix} -K_p I & -K_d I \end{bmatrix} (x_t - x^*)$$

- However, if K is full, then LQR controller accounts for interdependence of state variables
- Also, it can be much more intuitive to specify the cost function

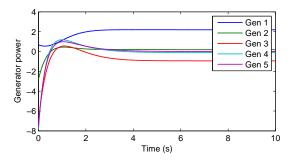
$$C(x_t, u_t) = ||Q(x_t - x^*)||_2^2 + ||R(u_t - u^*)||_2^2$$

than to guess control gains (cost specifies what we actually want to optimize)



Issues with LQR

- Sometimes, it is difficult to express the costs/constraints of a control task with just a quadratic cost function
- Control inputs from LQR controller



Inputs are similar for the above PD/PID controller

- LQR cannot enforce bounds on control inputs, cannot enforce hard constraints on resulting states
- Some heuristics for dealing with these issues
 - Take LQR controls and clip them to allowable region
 - Tune quadratic penalties (possibly varying over time), to ensure desired behavior
- Ultimately, little can be said about how well these methods will perform

Control via Optimization

- An alternative solution: return to the paradigm of control as optimization
- Recall LQR was just solving the (convex) optimization problem

minimize
$$\sum_{x_{1:T}, u_{1:T}}^{H} \left(\|Qx_t\|_2^2 + \|Ru_t\|_2^2 \right)$$
subject to
$$x_{t+1} = Ax_t + Bu_t$$
$$x_1 = x_{\text{init}}$$

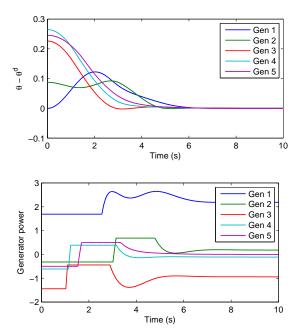
 We can easily augment this to include explicit bounds on states and controls

minimize
$$\sum_{t=1}^{H} (\|Qx_t\|_2^2 + \|Ru_t\|_2^2)$$
subject to
$$x_{t+1} = Ax_t + Bu_t$$
$$x_1 = x_{\text{init}}$$
$$\underline{u} \le u_t \le \overline{u}, \ \underline{x} \le x_t \le \overline{x}$$

 This is a Quadratic Program, can solve using YALMIP or specialized solvers \bullet Example: generator control with power limited to nominal power output ± 0.5 p.u.

```
x = sdpvar(2*N, T);
u = sdpvar(N, T);
C = [x(:,2:end) == A*x(:,1:end-1) + B*u(:,1:end-1) + a;
    x(:,1) == [zeros(n,1); omega_ref*ones(N,1)];
    u_star - 0.5 <= u;
    u_star + 0.5 >= u;]
solvesdp(C, norm(x-x_star,'fro')^2 + ...
    1e-3*norm(u-u_star,'fro')^2);
```

- Takes about 10 seconds to solve with YALMIP (for T=10000)
- Output is a sequence of optimal control actions $u_{1:T}$, not a feedback controller $u_t = Kx_t$



 Many advantages and disadvantages to PID, LQR, and optimization (many others in addition to these)

| | Pros | Cons |
|-----|-----------------------------|---------------------------|
| PID | Easy to implement (even | Gain tuning can be "art"; |
| | without model) | cannot always apply to |
| | | multi-variate systems |
| LQR | Gives feedback controller | Can't incorporate con- |
| | $u_t = Kx_t$; easy to com- | straints; requires model |
| | pute (with MATLAB) | |
| Opt | Can incorporate con- | More time consuming; |
| | straints; directly solves | doesn't give feedback |
| | optimal control problem | controller |