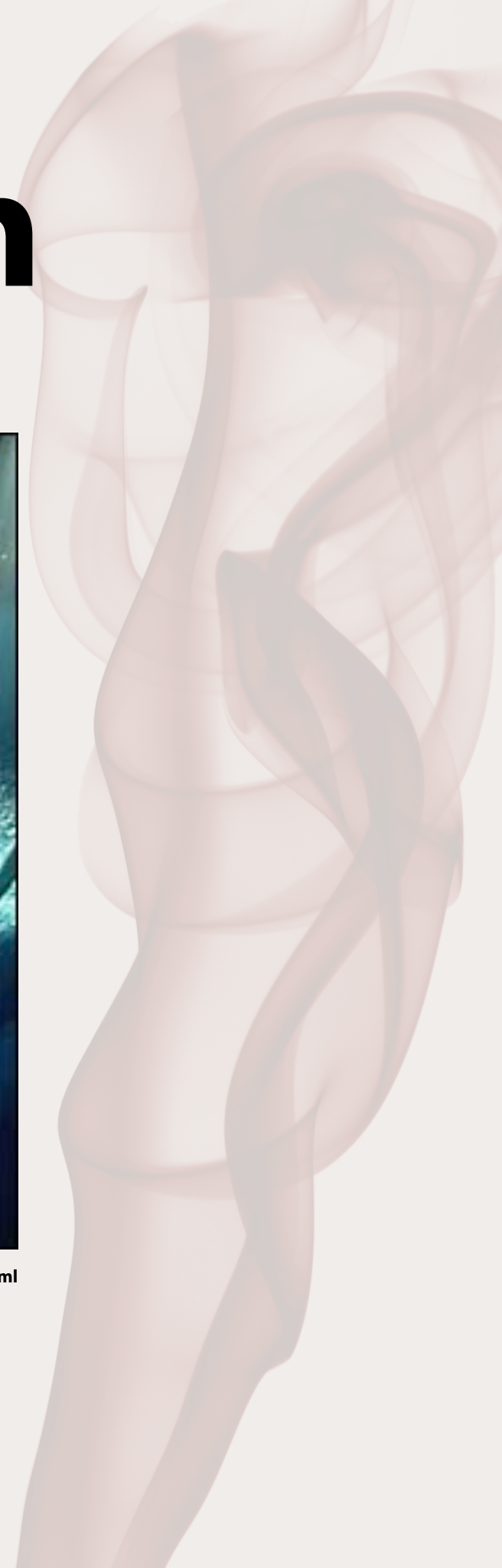


# Human Motion



source: [http://scaq.blogspot.com/2006\\_11\\_01\\_archive.html](http://scaq.blogspot.com/2006_11_01_archive.html)

**Adrien Treuille**



# Overview

- **Data-Driven Motion**
- **Physics Based Motion**
- **Motion of other Animals**
- **Questions**



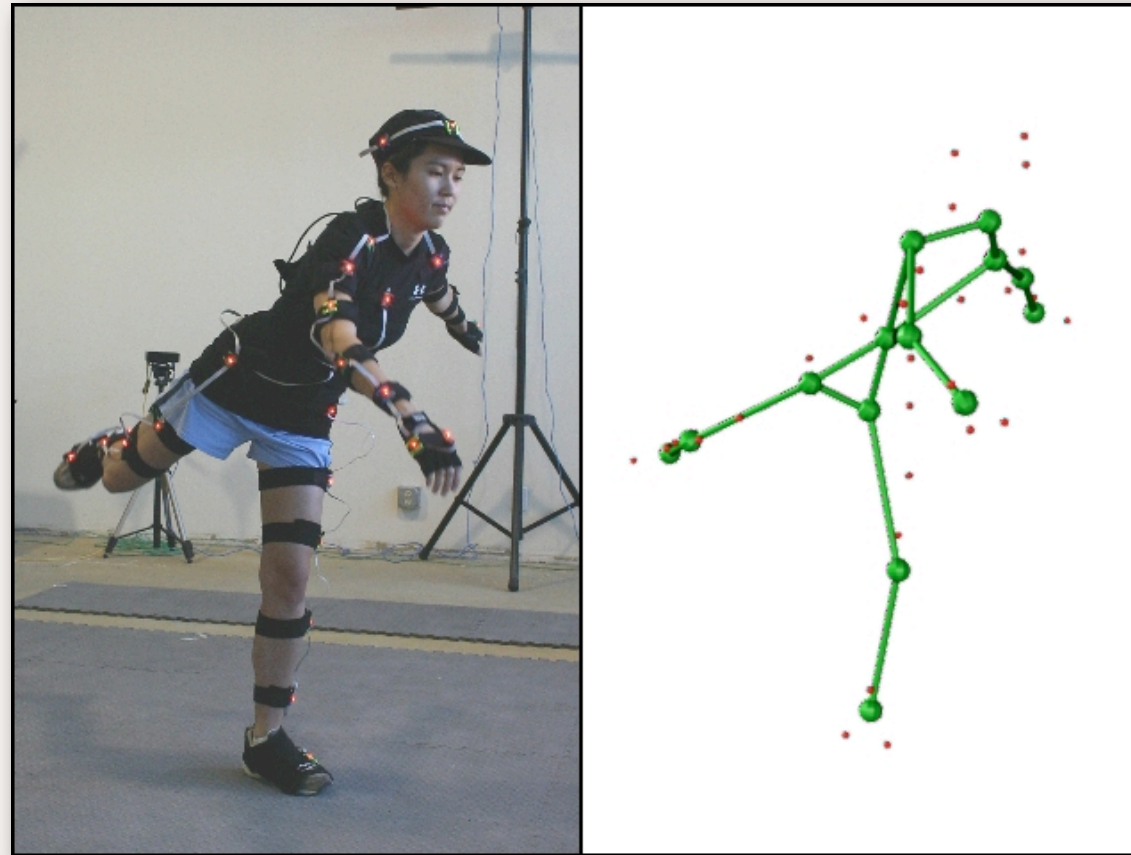
# Overview

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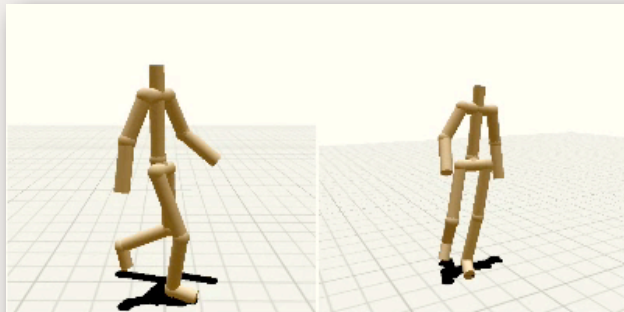


# Motion Capture

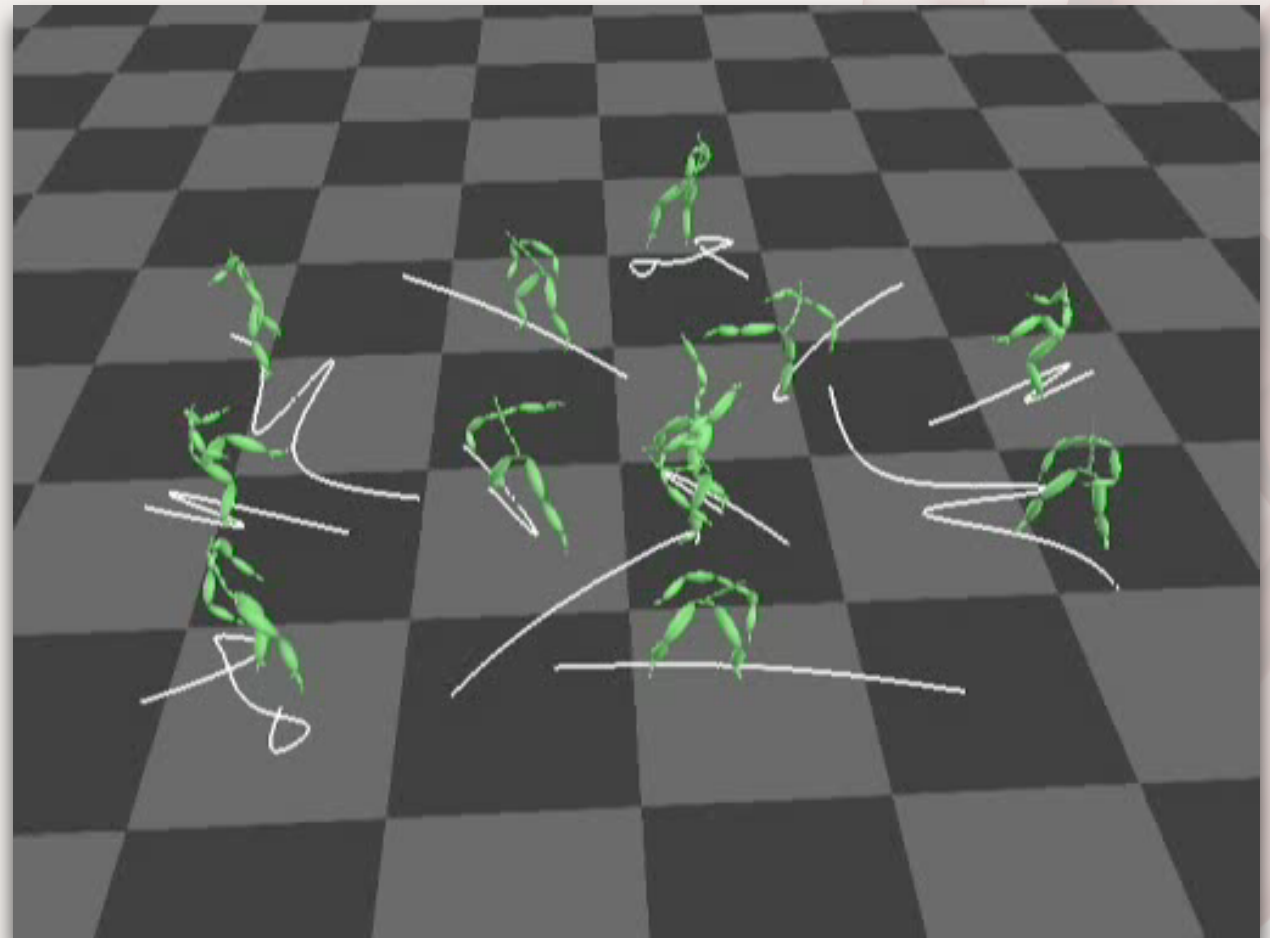


- **Telescoping composition of functions from root.**
- **Compute derivatives in the *opposite* direction!**

# Clips

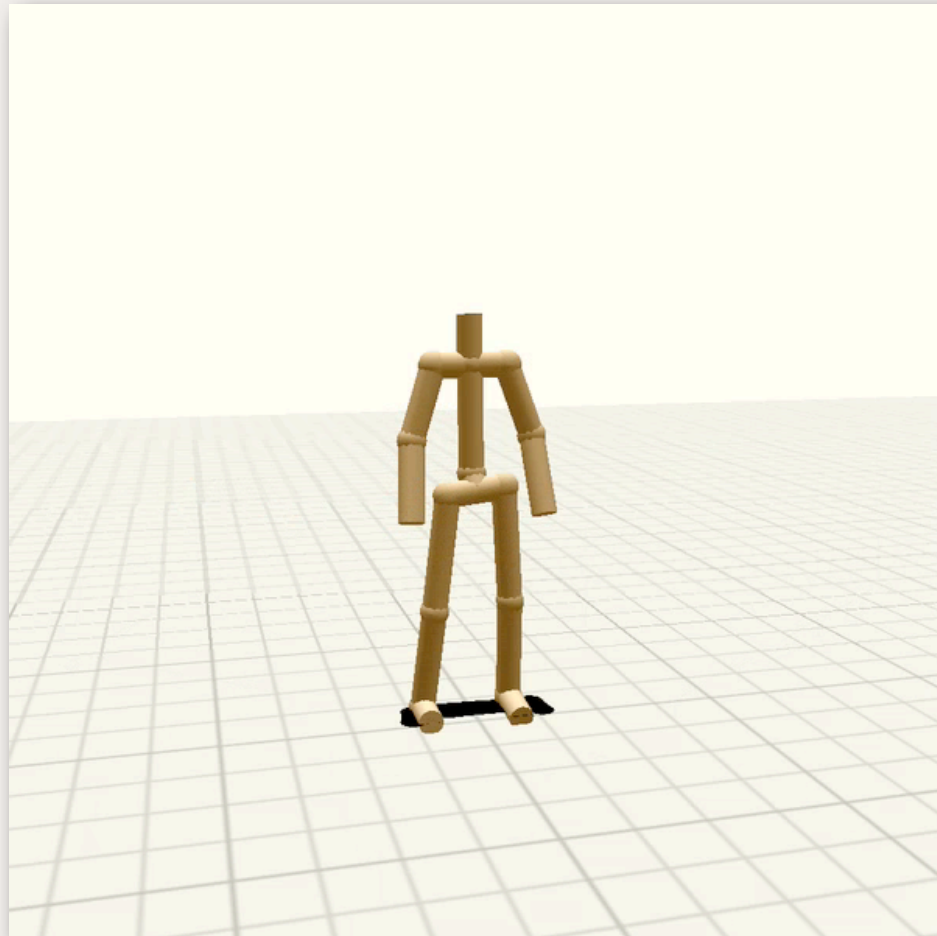


source: Treuille et al. [2002]

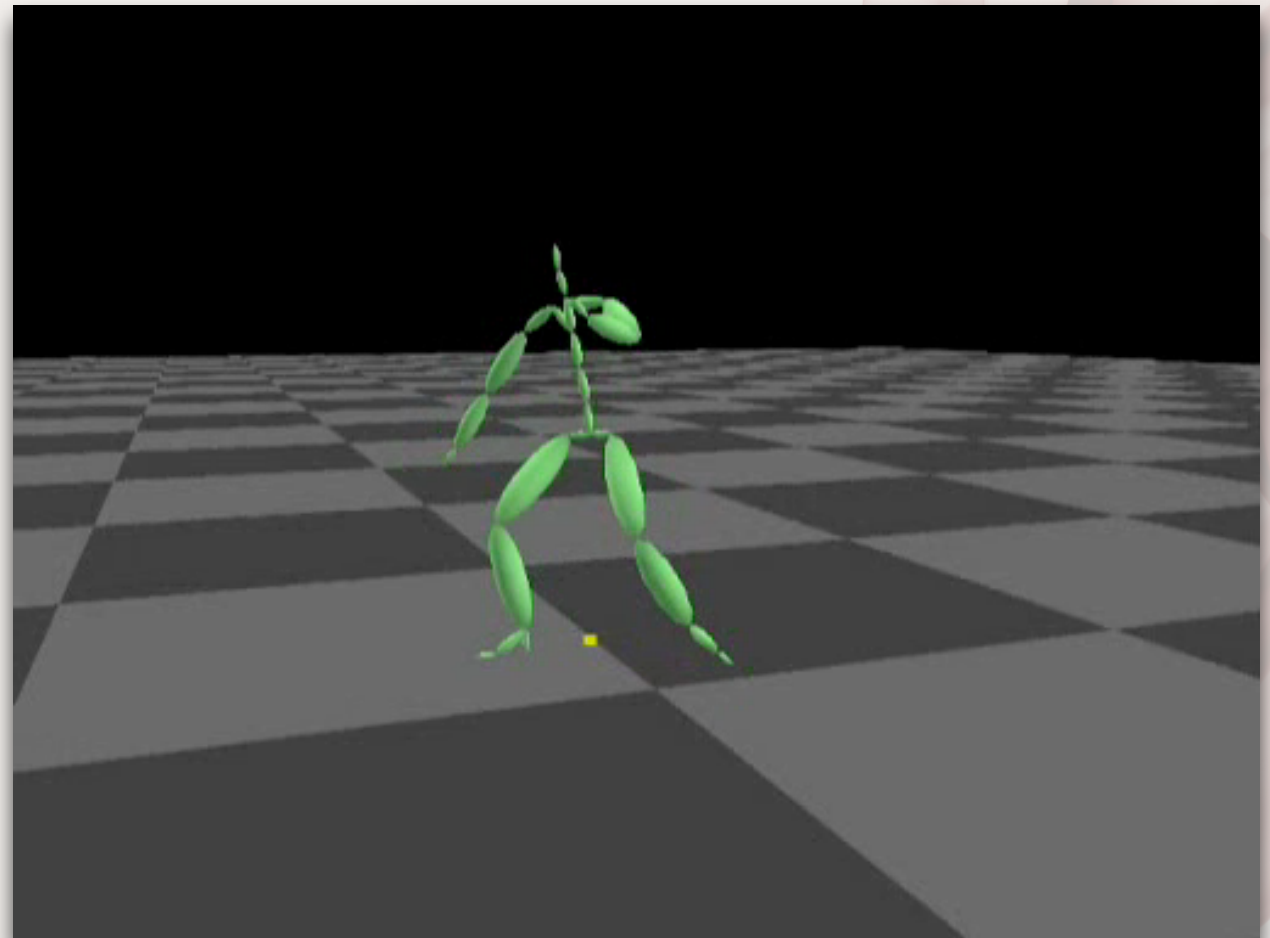


source: Kovar et al. [2002]

# Sequences



source: Treuille et al. [2002]

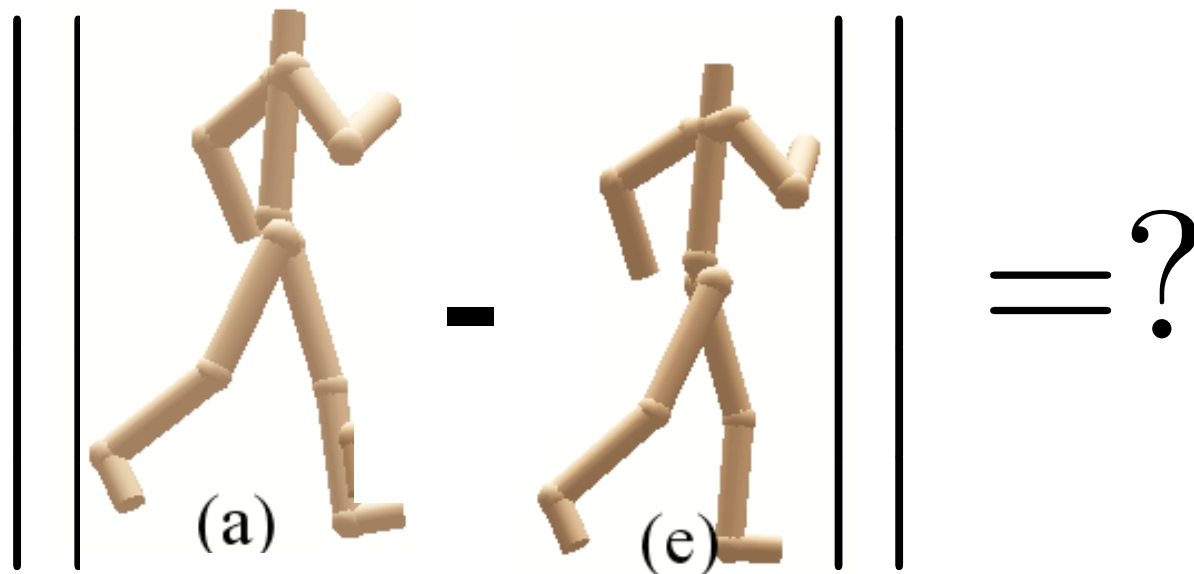


source: Kovar et al. [2002]

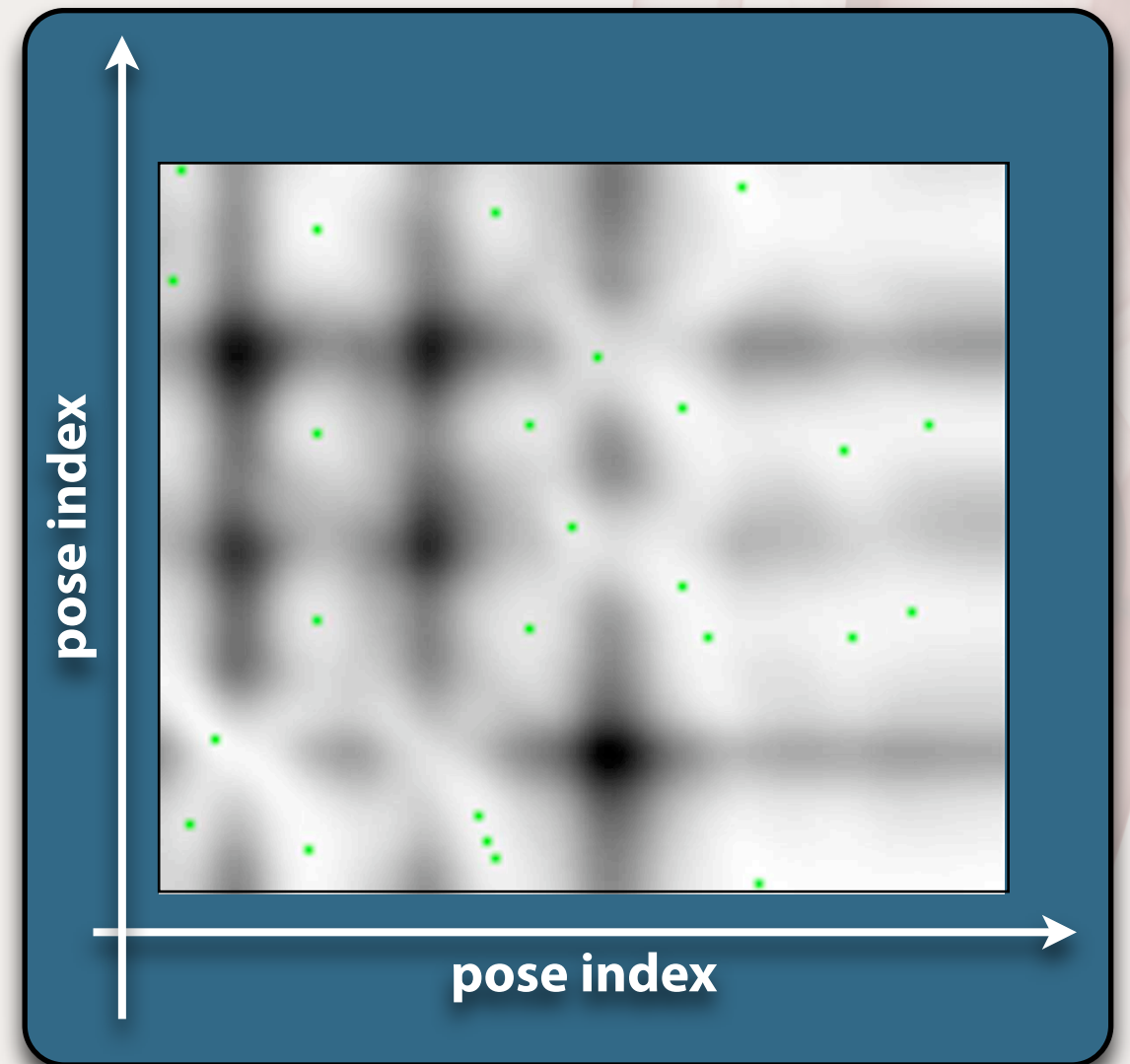
## How?



# Pose Metrics

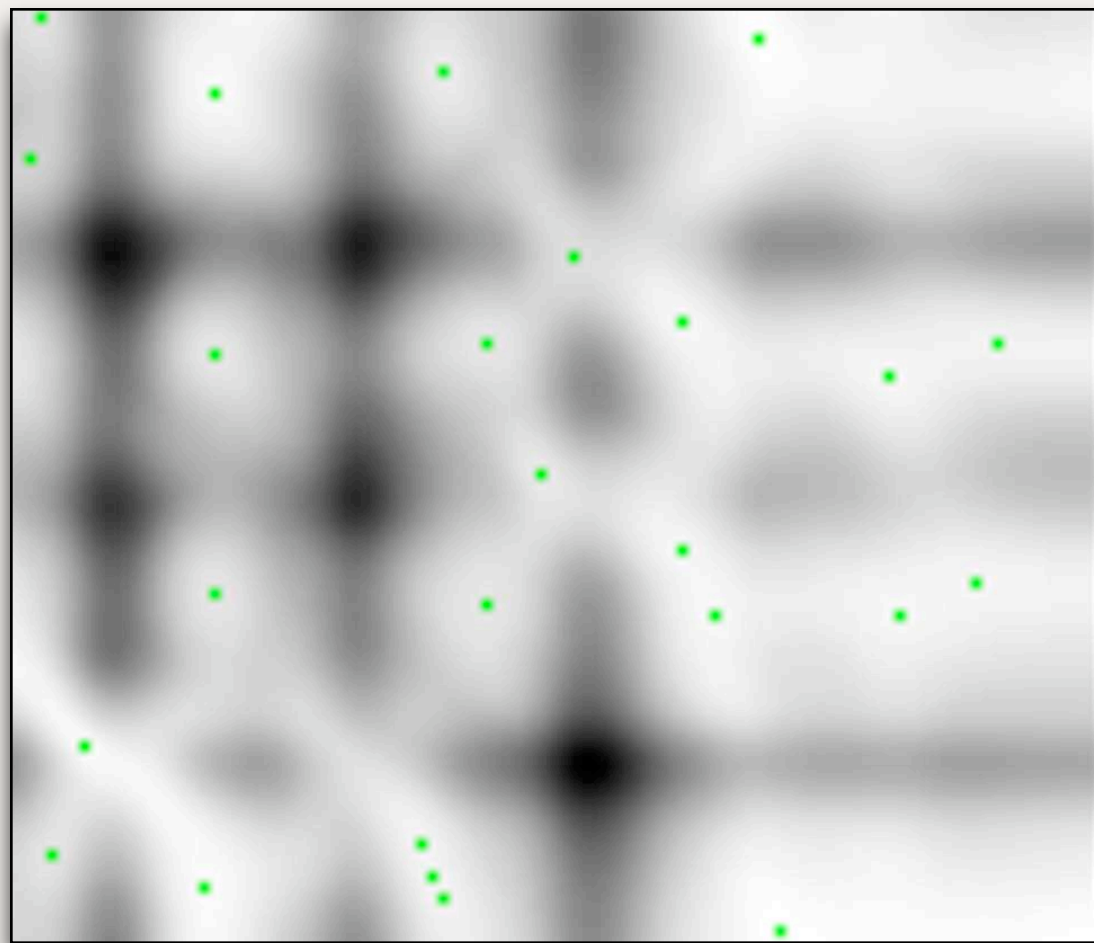


**How can we define  
a metric on poses?**

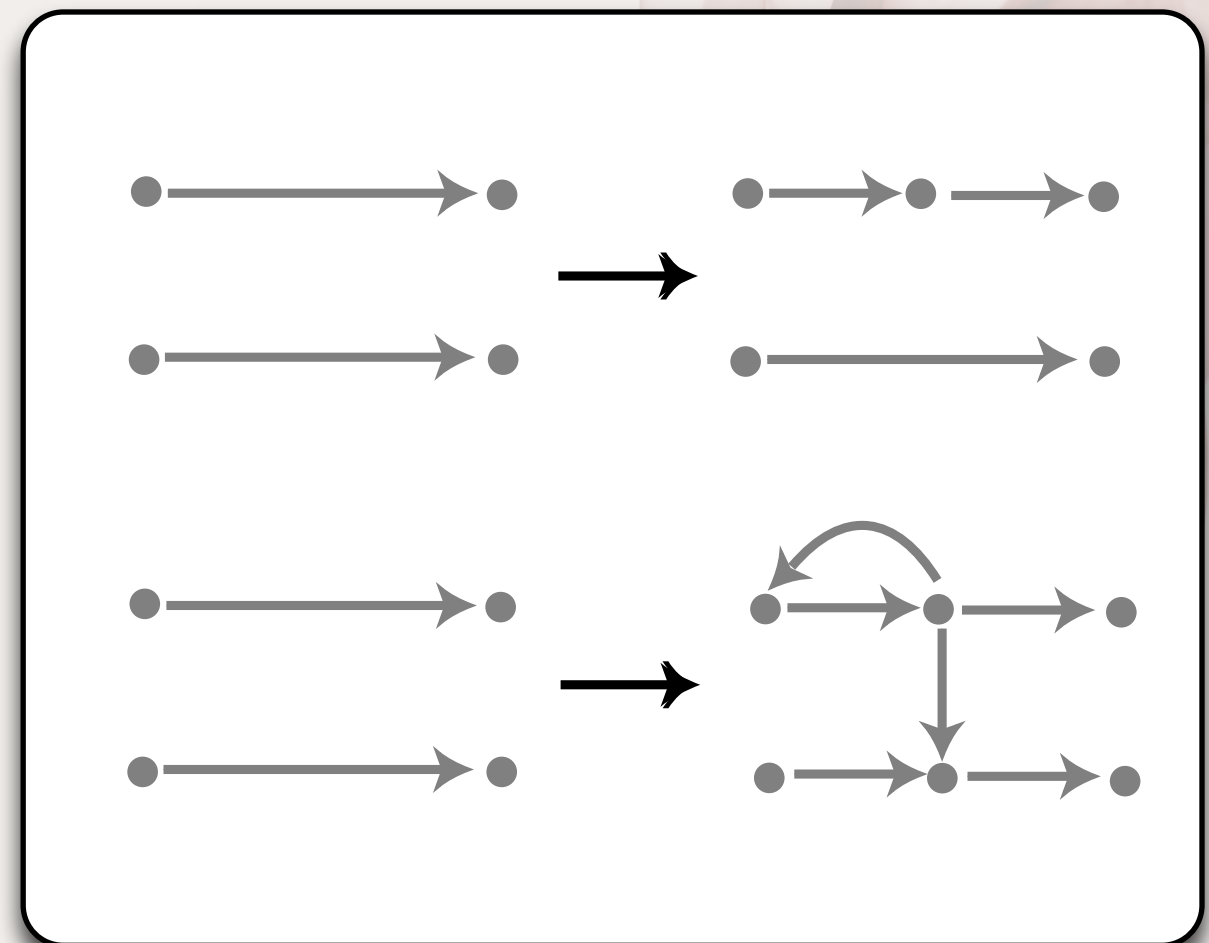
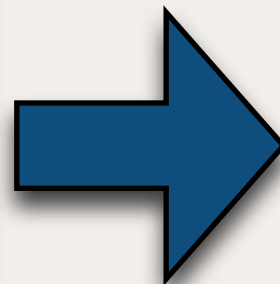


**Pairwise pose  
differences.**

# Pose Metrics



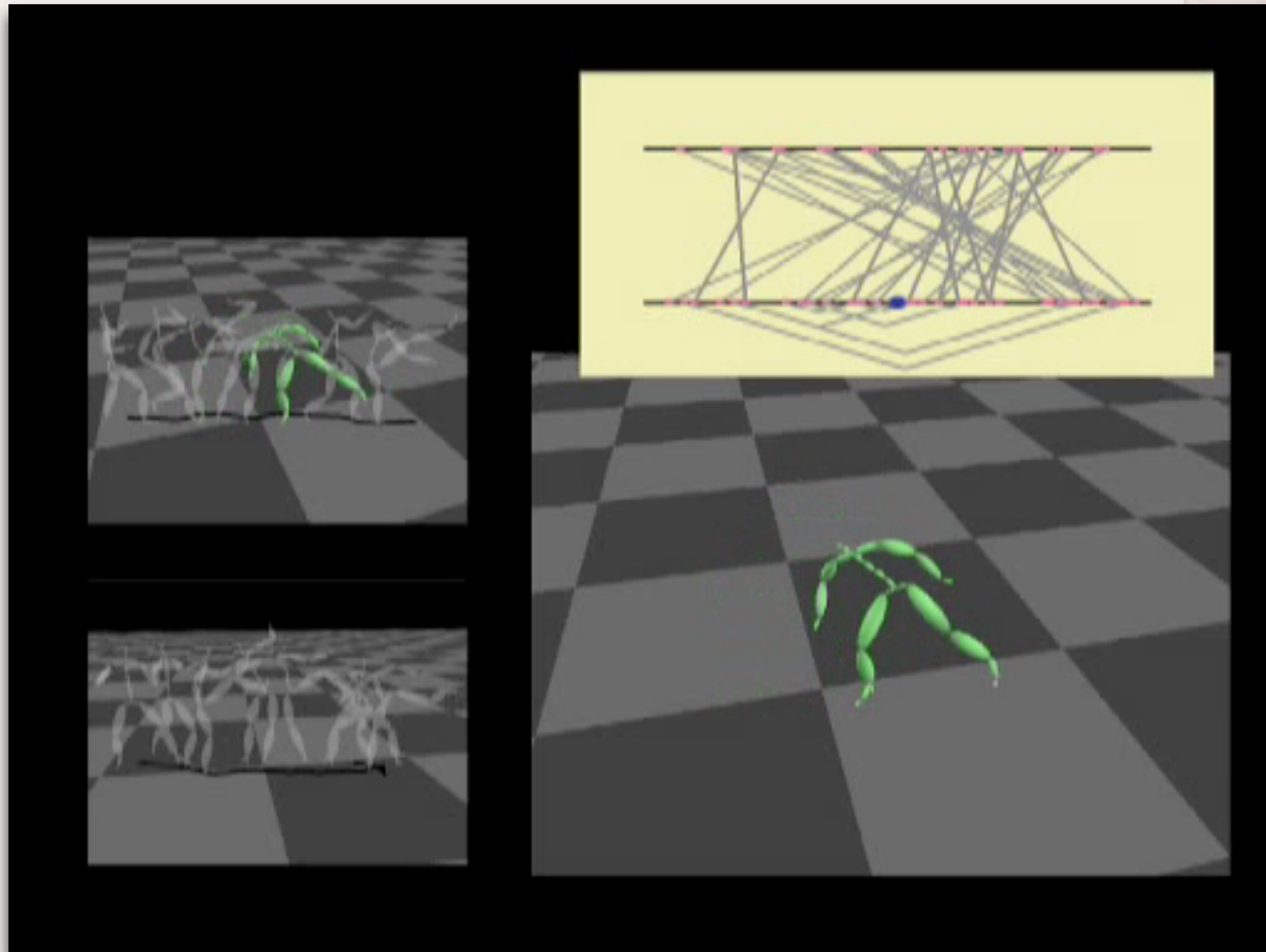
**Pairwise Pose Differences**



**Motion Graph Schematic**



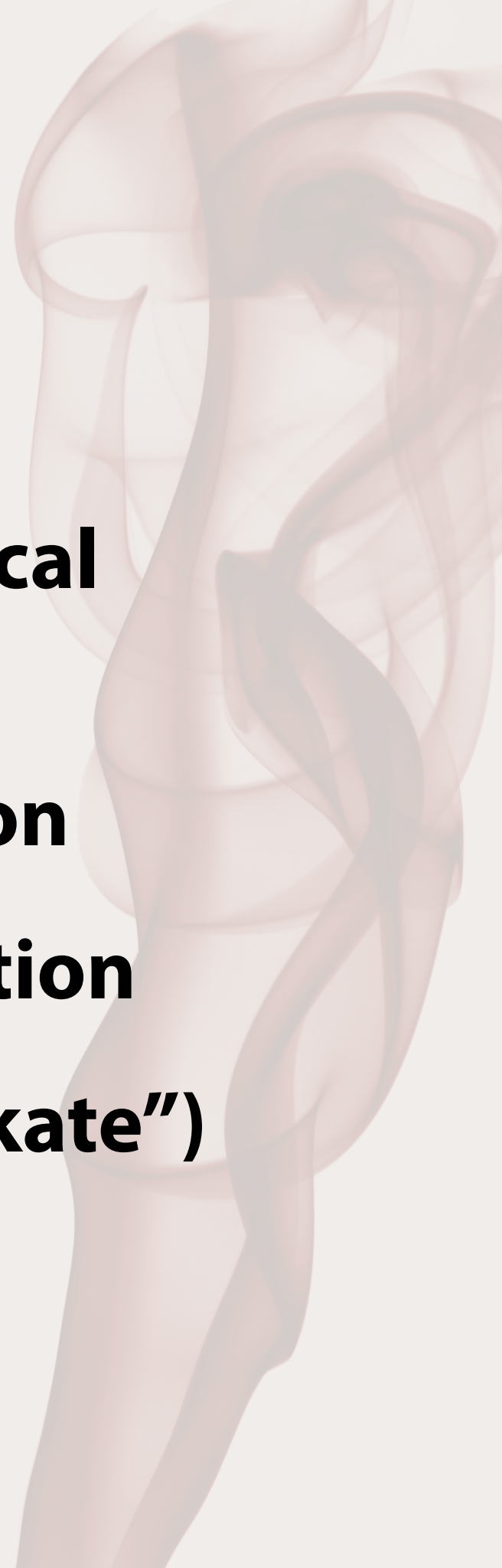
# Results



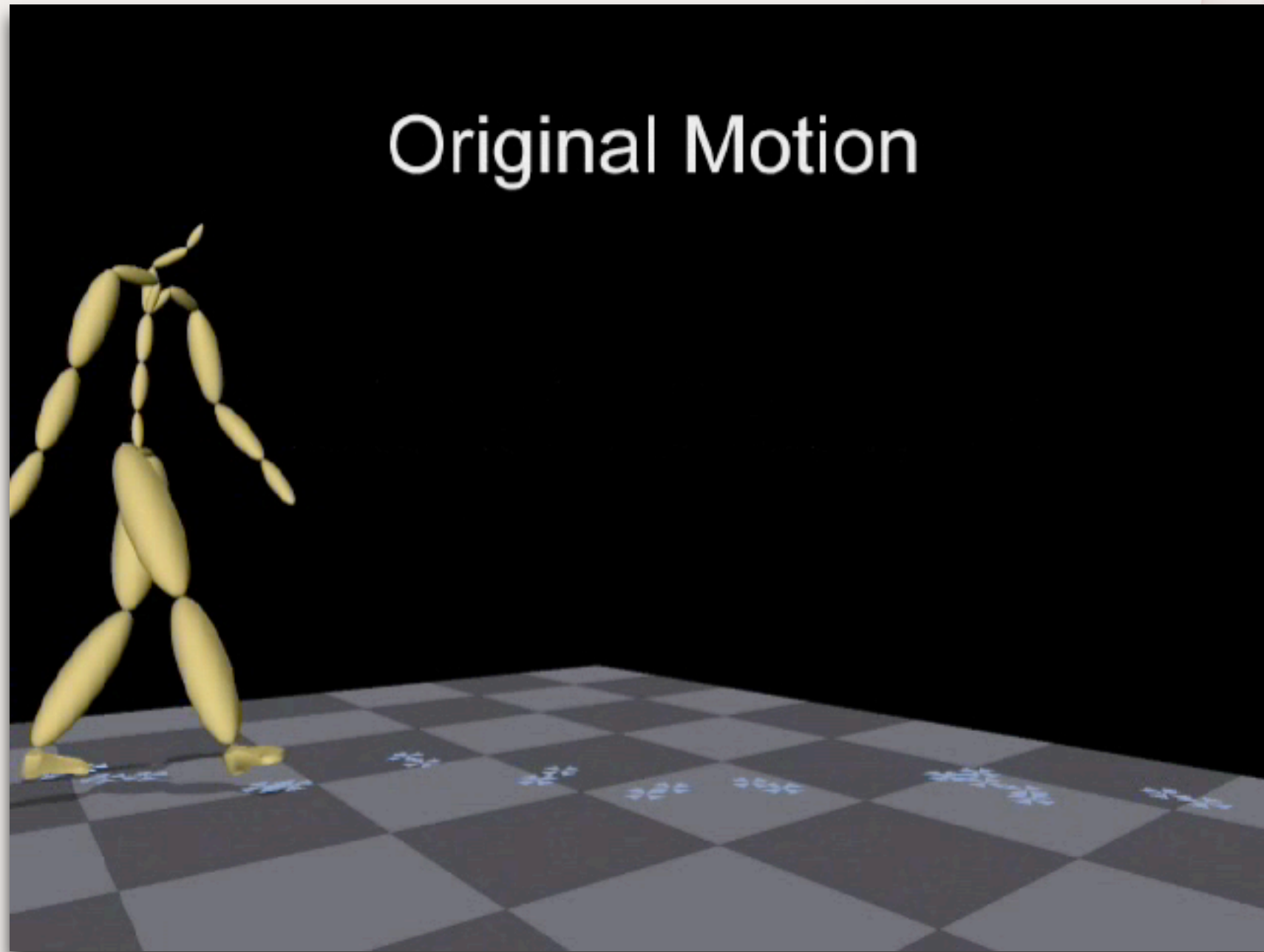
source: Kovar et al. [2002]

# Constraints

- **Pose blending may violate physical constraints**
- **Linear Momentum Conservation**
- **Angular Momentum Conservation**
- **Frictional Constraints (“Foot Skate”)**



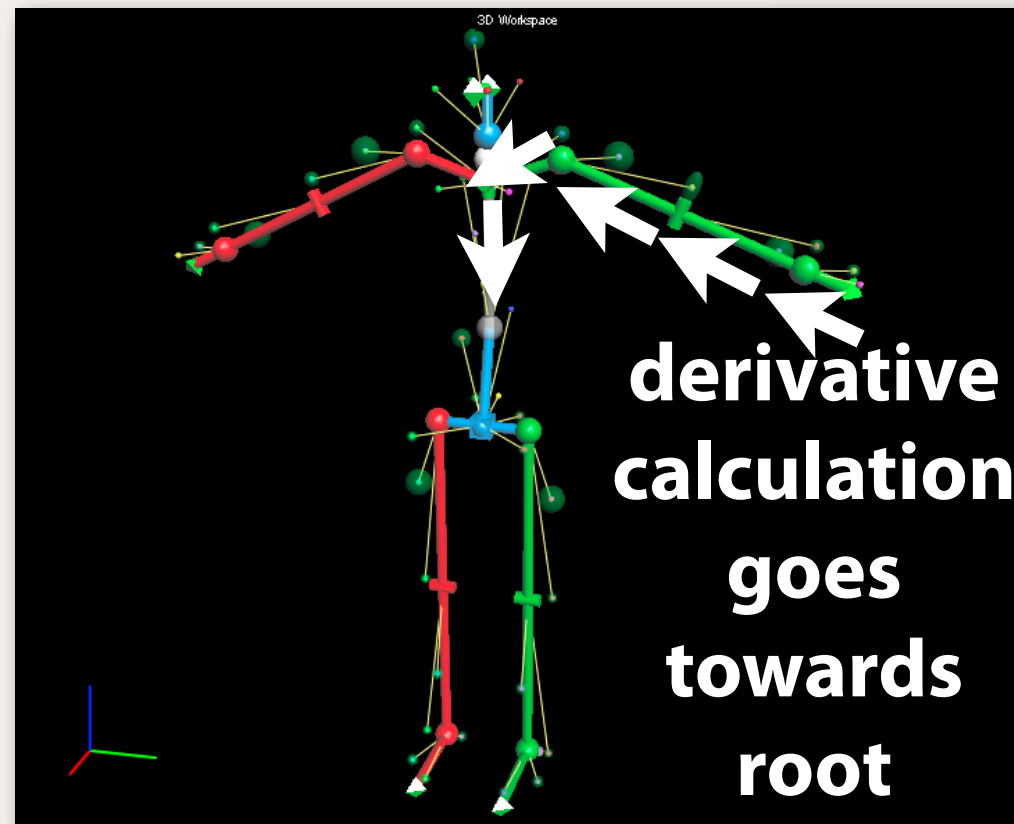
# “Foot Skate” Problem



source: <http://www.cs.wisc.edu/graphics/Gallery/kovar.vol/Cleanup/>



# Inverse Kinematic Solution

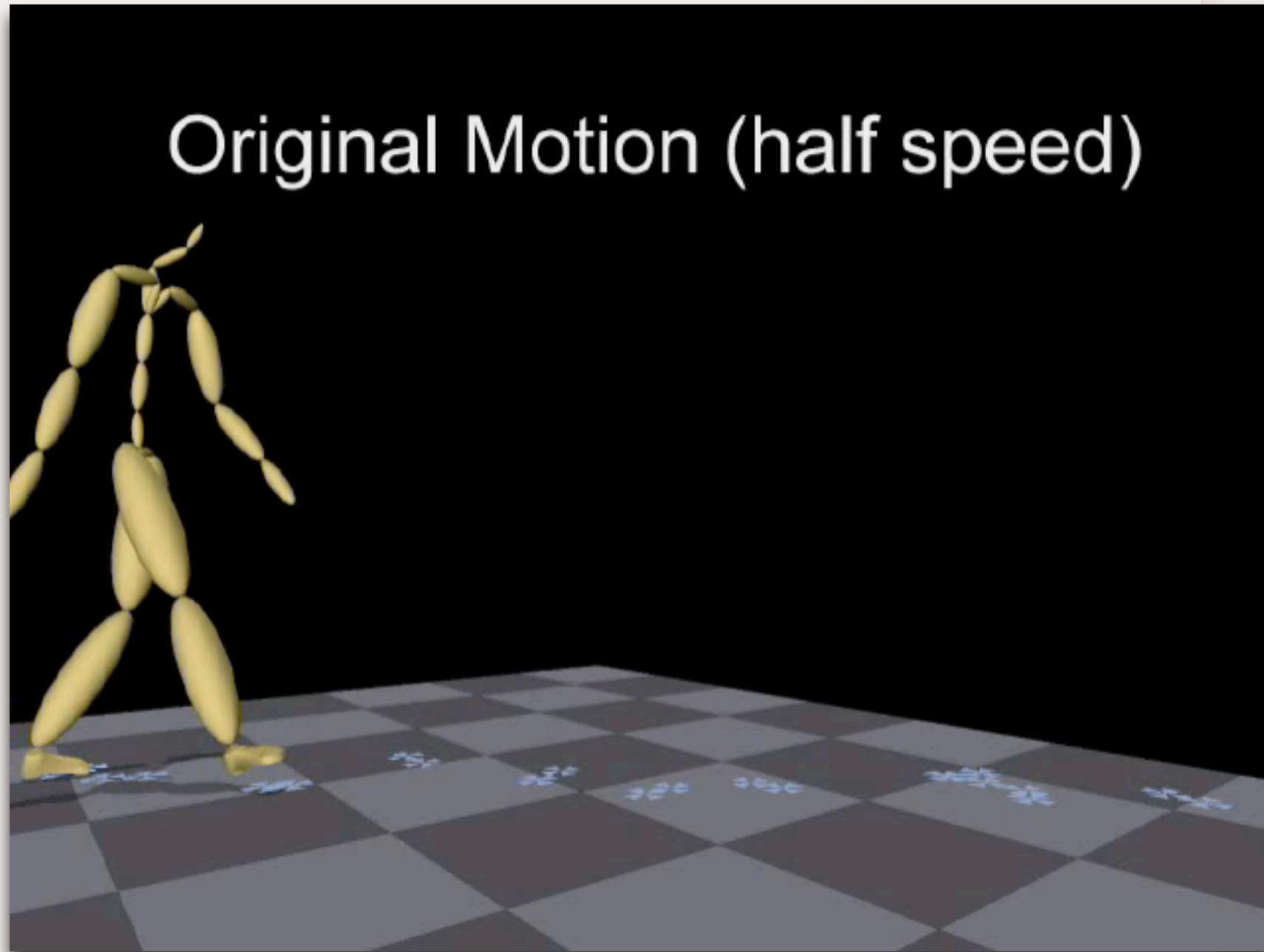


$$\omega_i = f_{i,\Omega}(\omega_{i-1})$$

$$\frac{dE}{d\Omega} = 2 \sum_j (\hat{\mathbf{m}}_j^* - \hat{\mathbf{m}}_j)^T \frac{d\hat{\mathbf{m}}_j}{d\Omega}$$

$$\frac{d\hat{\mathbf{m}}_j}{d\Omega} = \frac{\partial \hat{\mathbf{m}}_j}{\partial \omega_i} \left( \frac{\partial \omega_i}{\partial \Omega} + \frac{\partial \omega_i}{\partial \omega_{i-1}} \frac{\partial \omega_{i-1}}{\partial \Omega} + \frac{\partial \omega_i}{\partial \omega_{i-1}} \frac{\partial \omega_{i-1}}{\partial \omega_{i-2}} \frac{\partial \omega_{i-2}}{\partial \Omega} + \dots \right)$$

# IK Results

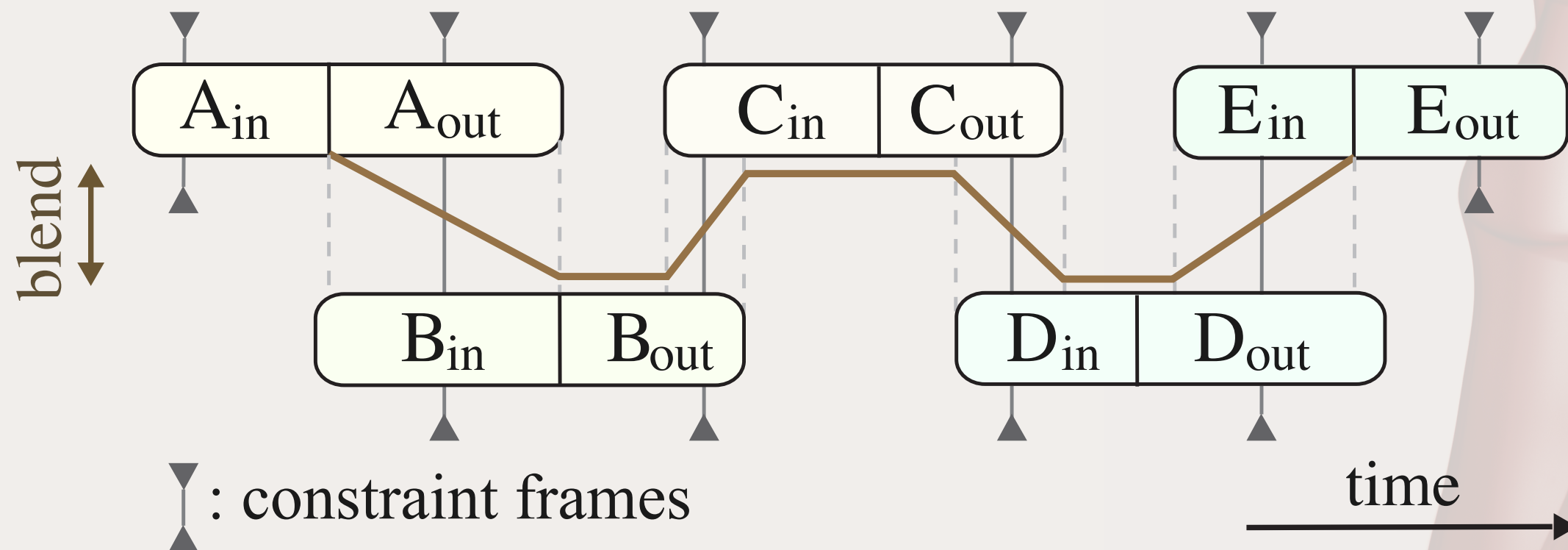
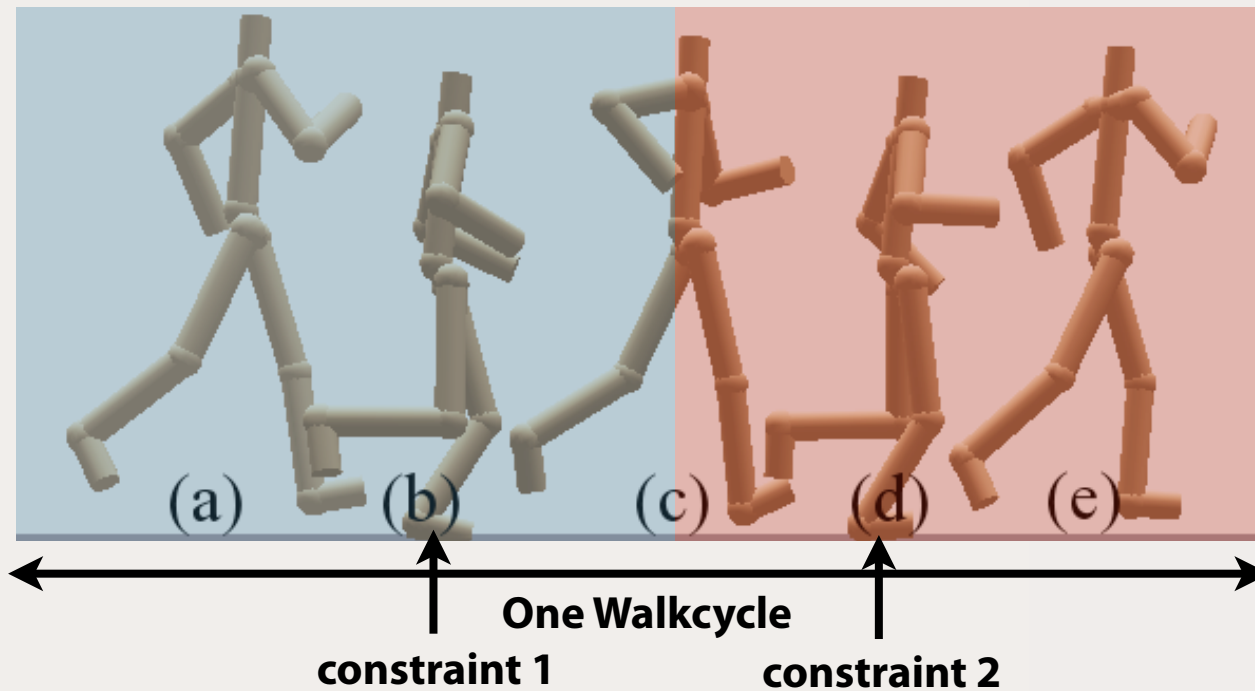


source: <http://www.cs.wisc.edu/graphics/Gallery/kovar.vol/Cleanup/>

# Smart Blending

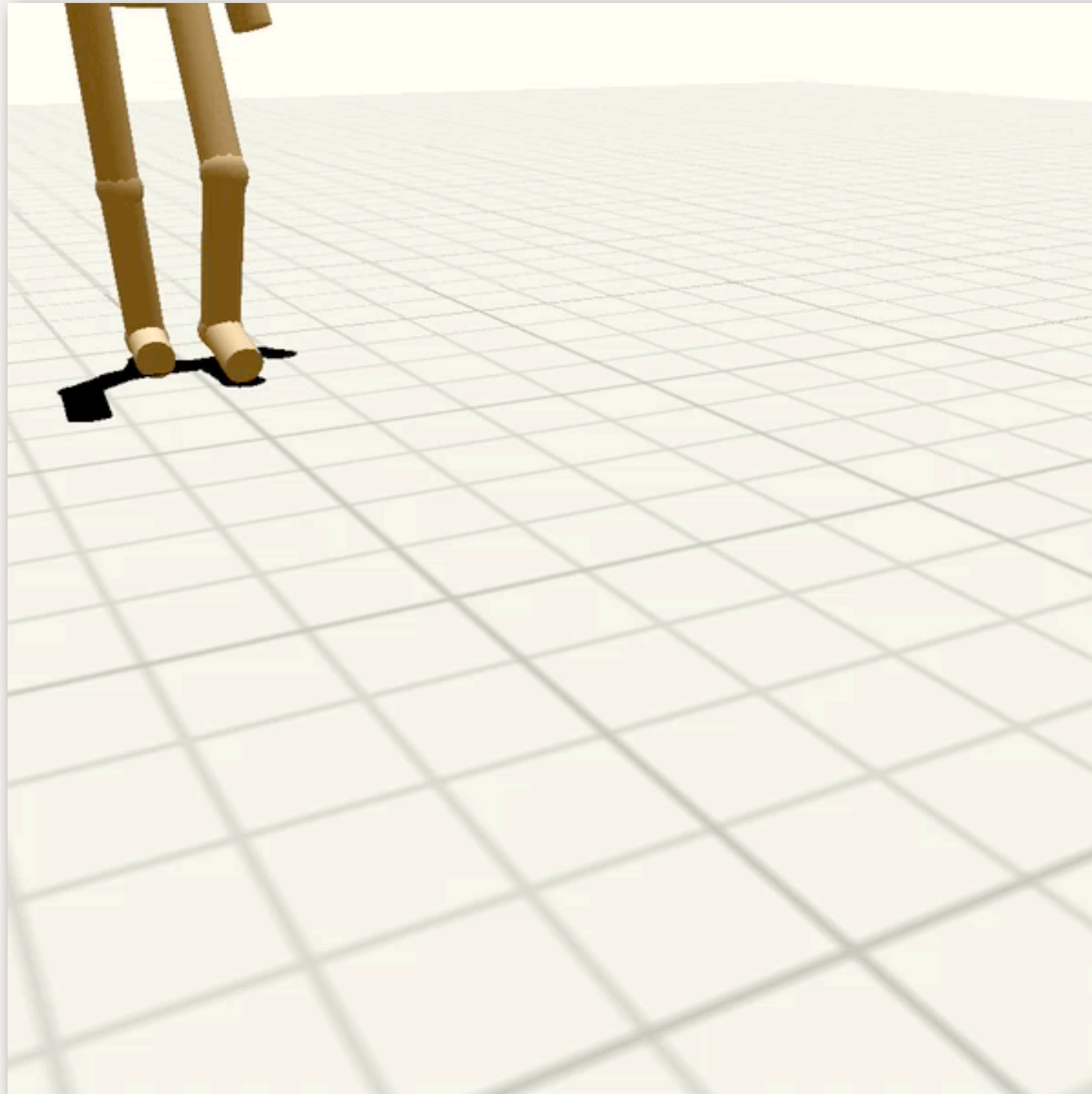
In Phase

Out Phase





# Smart Blending Example

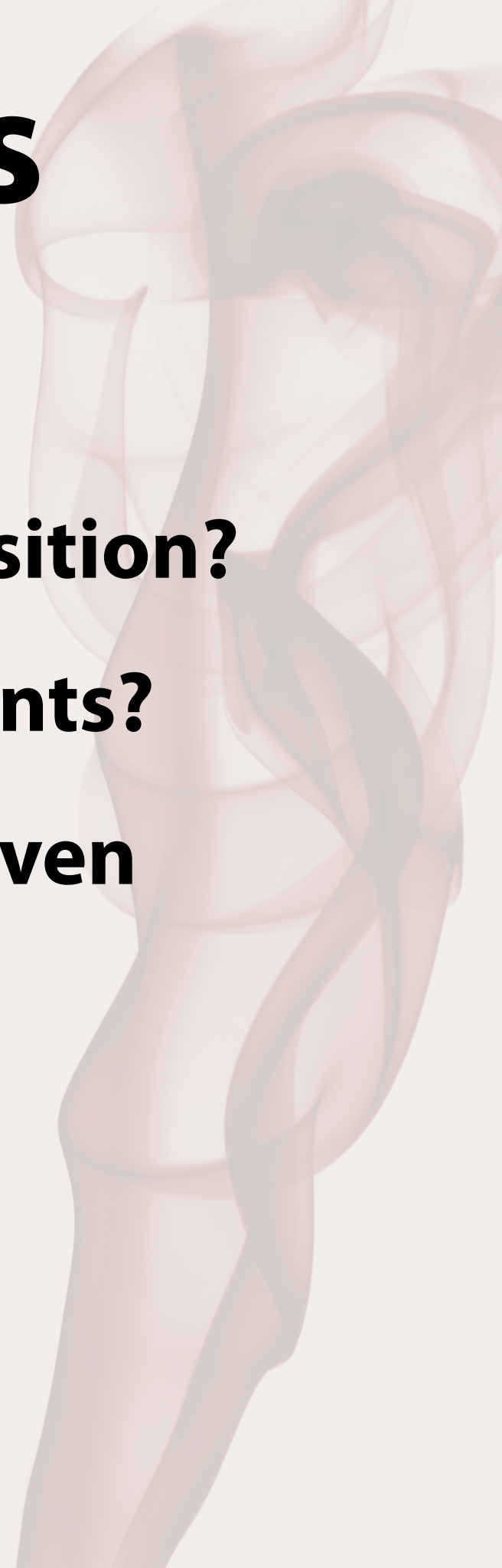


source: Treuille et al. [2002]



# Open Problems

- **How to pick to which clip to transition?**
- **How to enforce temporal constraints?**
- **How to generalize beyond the given clips?**



# Overview

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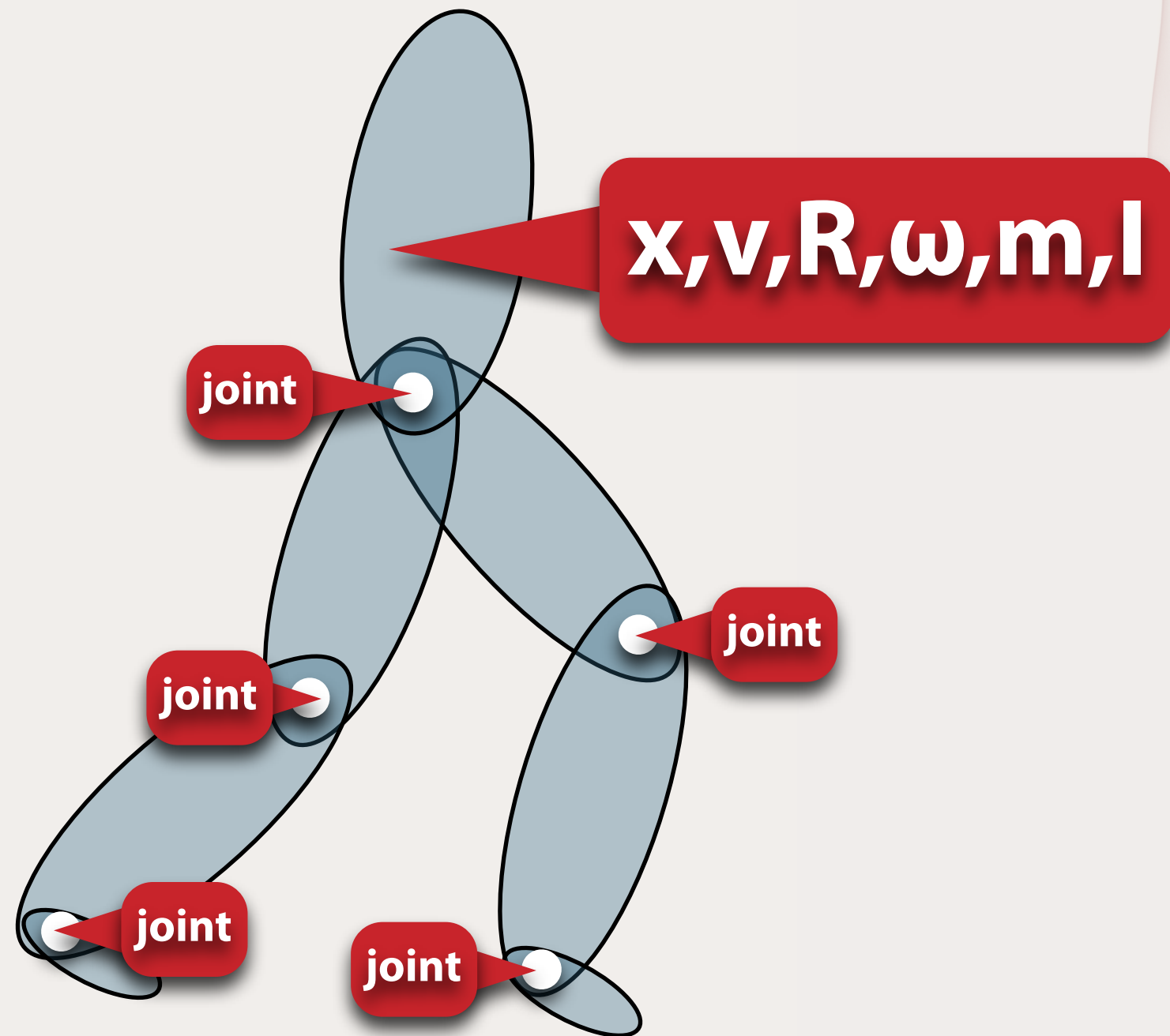


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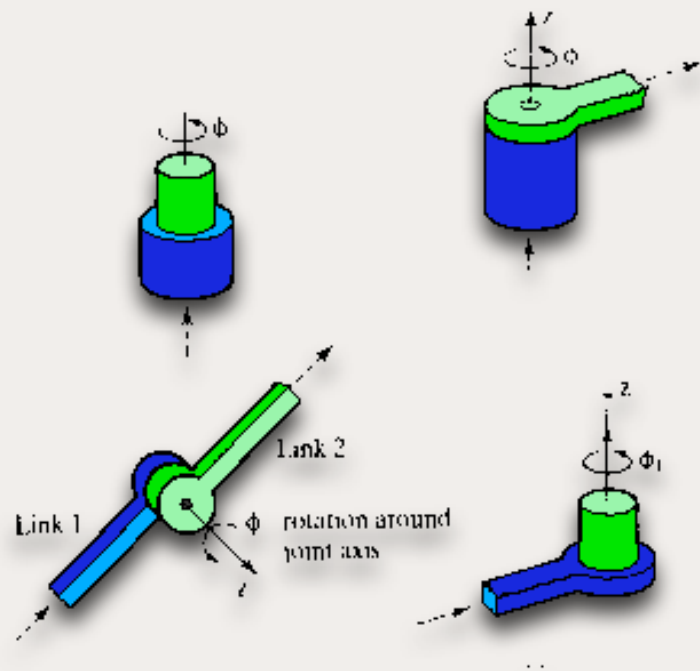


# Physical Model

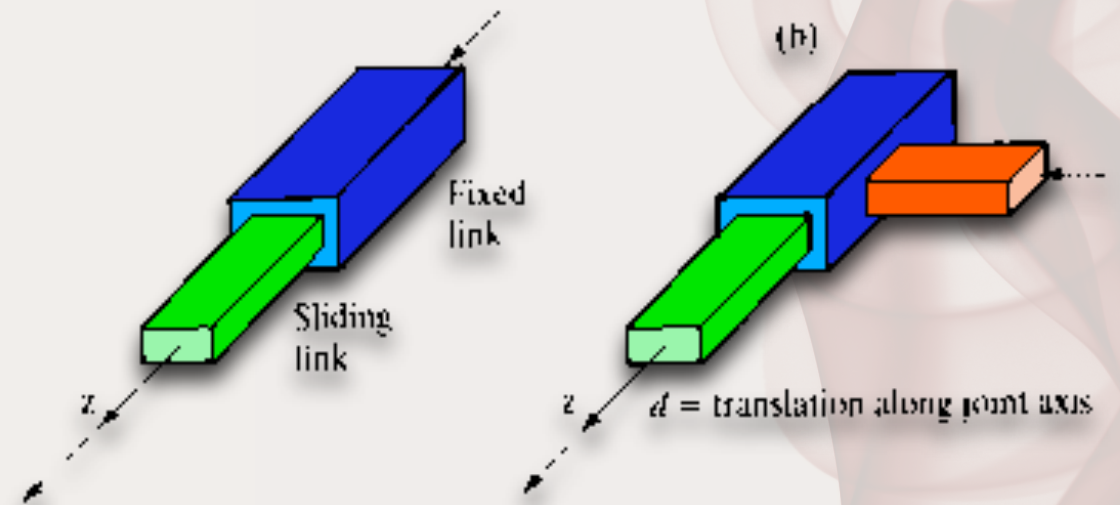


# Joint Types

**All joints can be written as the composition of...**



**Rotary**



**Prismatic**

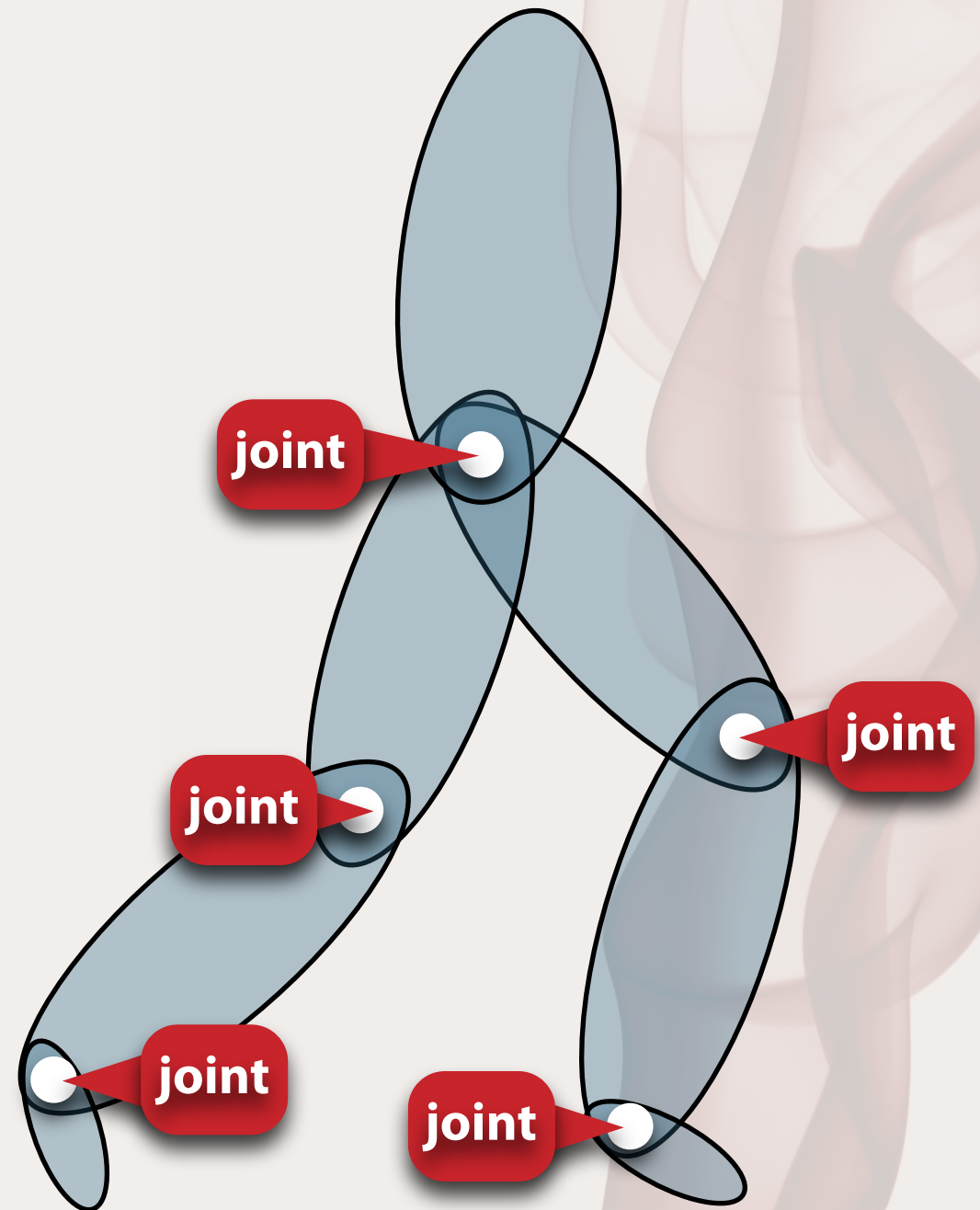
**...and have two forms:**

- 1. Constraint Form**
- 2. Functional Form**



# Joint Enforcement

- **Penalty Methods**
- **Constraint Methods**
  - aka Maximal Coordinate
- **Minimal Coordinates**



# Internal Coordinates

- $q$ : the skeletal coordinates
- $\dot{q}$ : joint velocities
- $\ddot{q}$ : joint accelerations

- ***Forward Dynamics Problem***

- **Compute  $\ddot{q} = F(q, \dot{q}, f, \tau)$**

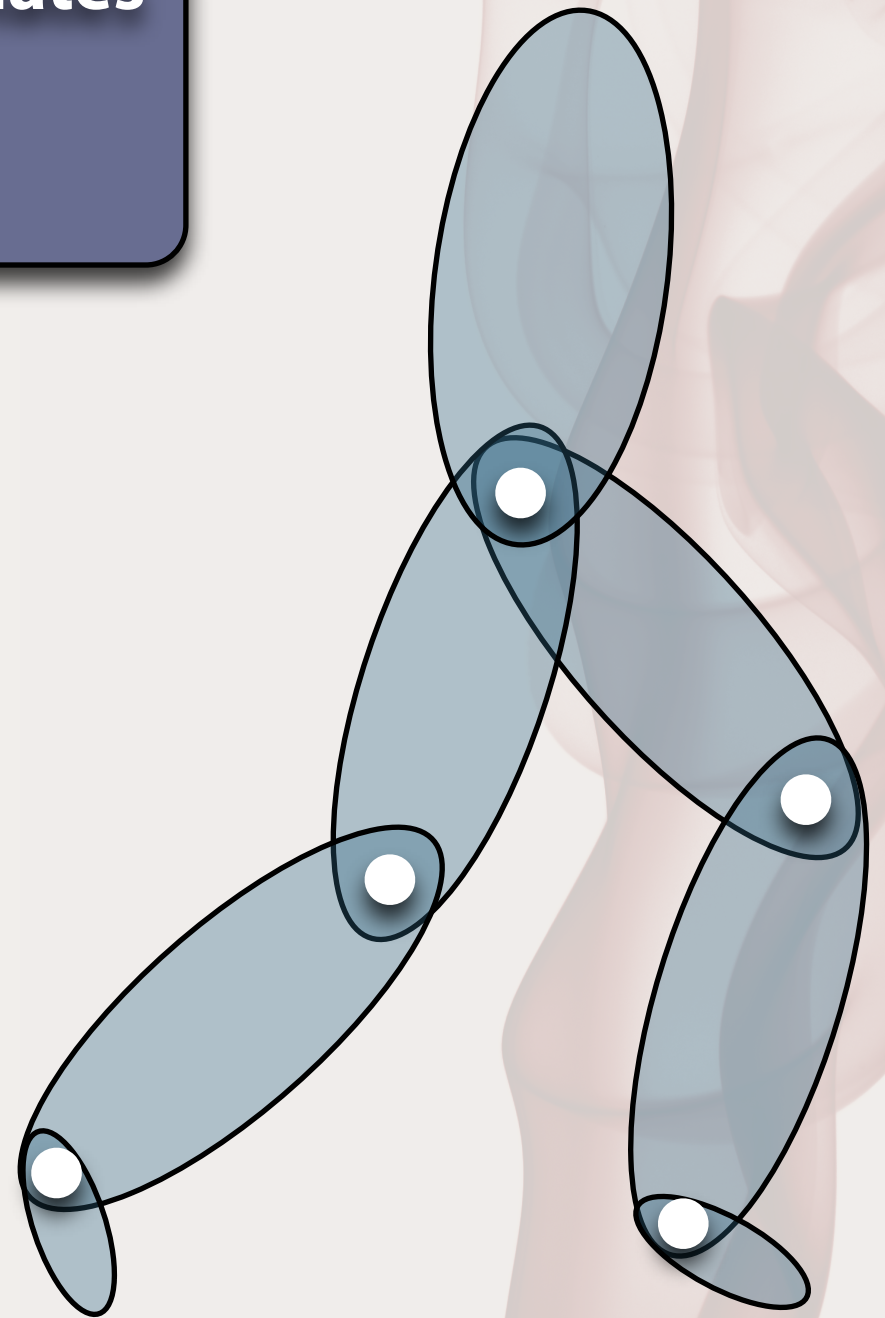
- $f$ : external forces

- $\tau$ : internal torques

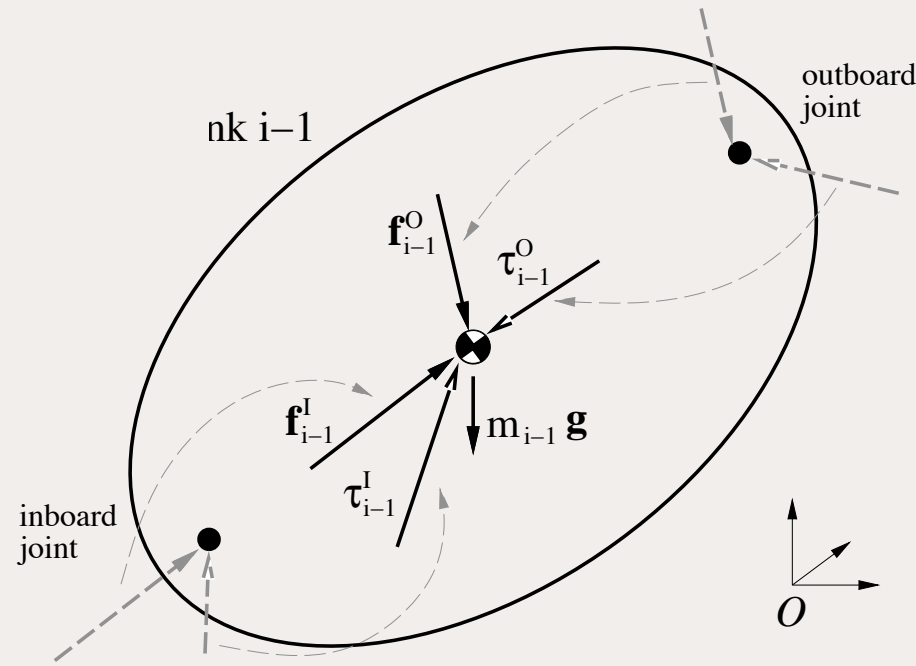
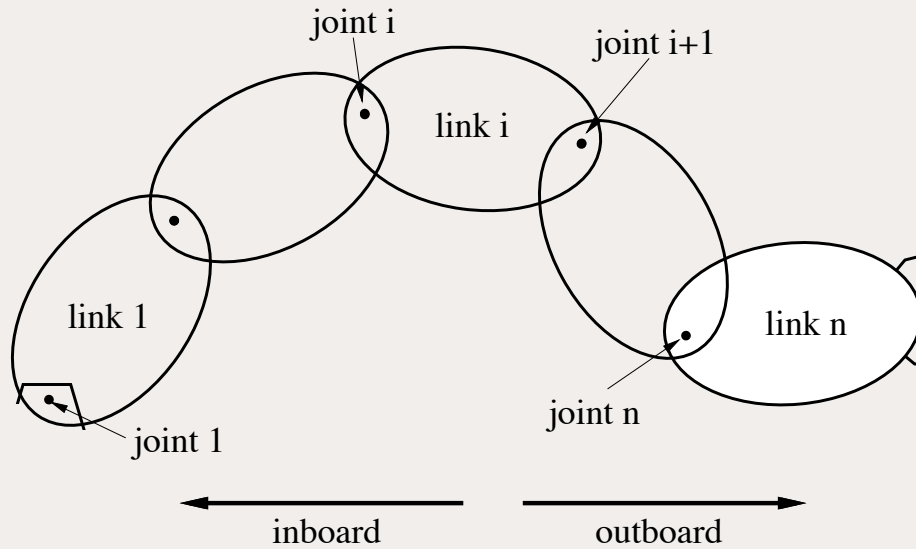
- **Then use ODE solver.**

- ***Inverse Dynamics Problem***

- **Compute  $\tau = G(q, \dot{q}, \ddot{q}, f)$**



# Featherstone Algorithm



## Impulse-based Dynamic Simulation of Rigid Body Systems

by

Brian Vincent Mirtich

If joint  $i$  is prismatic,

$$\dot{\mathbf{s}}_i' \hat{\mathbf{f}}_i^I = \begin{bmatrix} \mathbf{0} \\ \mathbf{u}_i \end{bmatrix}' \begin{bmatrix} \mathbf{f} \\ \boldsymbol{\tau} - \mathbf{d}_i \times \mathbf{f} \end{bmatrix} = \mathbf{f} \cdot \mathbf{u}_i.$$

The right hand side is the component of the applied force along the joint axis. This force must be supported by the actuator, hence, it is  $Q_i$ . If joint  $i$  is revolute,

$$\dot{\mathbf{s}}_i' \hat{\mathbf{f}}_i^I = \begin{bmatrix} \mathbf{u}_i \\ \mathbf{u}_i \times \mathbf{d}_i \end{bmatrix}' \begin{bmatrix} \mathbf{f} \\ \boldsymbol{\tau} - \mathbf{d}_i \times \mathbf{f} \end{bmatrix} = \mathbf{f} \cdot (\mathbf{u}_i \times \mathbf{d}_i) + (\boldsymbol{\tau} - \mathbf{d}_i \times \mathbf{f}) \cdot \mathbf{u}_i.$$

The right hand side reduces to  $\boldsymbol{\tau} \cdot \mathbf{u}_i$ , the component of the applied torque along the joint axis. This torque must be supported by the actuator, hence, it is  $Q_i$ .  $\square$

Substituting equation (4.23) for link  $i$ 's spatial acceleration into (4.24) yields

$$\hat{\mathbf{f}}_i^I = \hat{\mathbf{I}}_i^A (\hat{\mathbf{X}}_{i-1} \hat{\mathbf{a}}_{i-1} + \ddot{q}_i \mathbf{s}_i + \hat{\mathbf{c}}_i) + \hat{\mathbf{Z}}_i^A.$$

Premultiplying both sides by  $\dot{\mathbf{s}}_i'$  and applying Lemma 7 gives

$$Q_i = \dot{\mathbf{s}}_i' \hat{\mathbf{f}}_i^I (\hat{\mathbf{X}}_{i-1} \hat{\mathbf{a}}_{i-1} + \ddot{q}_i \mathbf{s}_i + \hat{\mathbf{c}}_i) + \dot{\mathbf{s}}_i' \hat{\mathbf{Z}}_i^A,$$

from which  $\ddot{q}_i$  may be determined:

$$\ddot{q}_i = \frac{Q_i - \dot{\mathbf{s}}_i' \hat{\mathbf{f}}_i^I \hat{\mathbf{X}}_{i-1} \hat{\mathbf{a}}_{i-1} - \dot{\mathbf{s}}_i' (\hat{\mathbf{Z}}_i^A + \hat{\mathbf{I}}_i^A \hat{\mathbf{c}}_i)}{\dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A \mathbf{s}_i}. \quad (4.27)$$

Substituting this expression for  $\ddot{q}_i$  into (4.26) and rearranging gives

$$\begin{aligned} \hat{\mathbf{f}}_{i-1}^I &= \left[ \hat{\mathbf{I}}_{i-1} + \hat{\mathbf{I}}_{i-1} \hat{\mathbf{X}}_i \left( \hat{\mathbf{I}}_i^A - \frac{\hat{\mathbf{I}}_i^A \dot{\mathbf{s}}_i \dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A}{\dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A \mathbf{s}_i} \right) \hat{\mathbf{X}}_{i-1} \right] \hat{\mathbf{a}}_{i-1} \\ &\quad + \hat{\mathbf{Z}}_{i-1}^A + \hat{\mathbf{I}}_{i-1} \hat{\mathbf{X}}_i \left[ \hat{\mathbf{Z}}_i^A + \hat{\mathbf{I}}_i^A \hat{\mathbf{c}}_i + \frac{\hat{\mathbf{I}}_i^A \mathbf{s}_i [Q_i - \dot{\mathbf{s}}_i' (\hat{\mathbf{Z}}_i^A + \hat{\mathbf{I}}_i^A \hat{\mathbf{c}}_i)]}{\dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A \mathbf{s}_i} \right]. \end{aligned}$$

Comparing this to the desired form (4.24),

$$\hat{\mathbf{I}}_{i-1}^A = \hat{\mathbf{I}}_{i-1} + \hat{\mathbf{I}}_{i-1} \hat{\mathbf{X}}_i \left( \hat{\mathbf{I}}_i^A - \frac{\hat{\mathbf{I}}_i^A \dot{\mathbf{s}}_i \dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A}{\dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A \mathbf{s}_i} \right) \hat{\mathbf{X}}_{i-1} \quad (4.28)$$

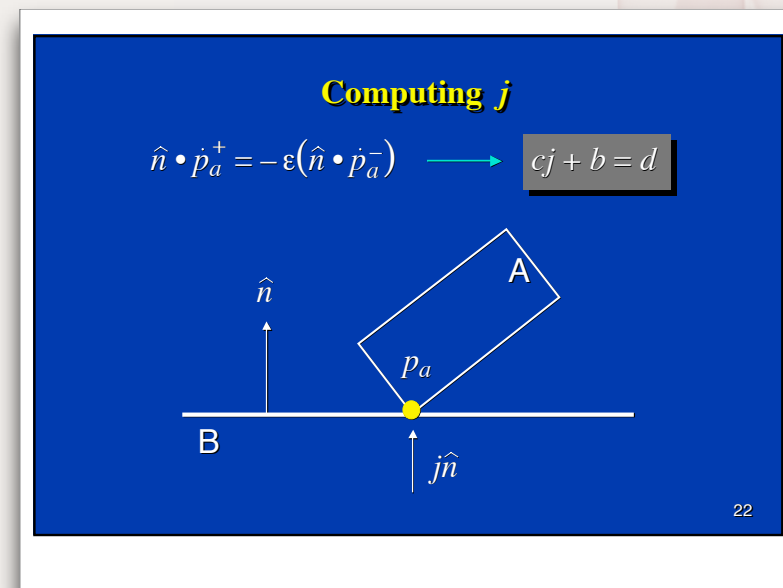
$$\hat{\mathbf{Z}}_{i-1}^A = \hat{\mathbf{Z}}_{i-1} + \hat{\mathbf{I}}_{i-1} \hat{\mathbf{X}}_i \left[ \hat{\mathbf{Z}}_i^A + \hat{\mathbf{I}}_i^A \hat{\mathbf{c}}_i + \frac{\hat{\mathbf{I}}_i^A \mathbf{s}_i [Q_i - \dot{\mathbf{s}}_i' (\hat{\mathbf{Z}}_i^A + \hat{\mathbf{I}}_i^A \hat{\mathbf{c}}_i)]}{\dot{\mathbf{s}}_i' \hat{\mathbf{I}}_i^A \mathbf{s}_i} \right]. \quad (4.29)$$



# Constraints

- Accelerations are *linear* in applied torques and forces.

$$a_f = k f + a_0$$



- Use of “test forces”
- Multiple test forces

$$\mathbf{a}_f = \mathbf{K} \mathbf{f} + \mathbf{a}_0$$

# Examples

## Efficient Synthesis of Physically Valid Human Motion

Anthony C. Fang

Nancy S. Pollard

Computer Science Department  
Brown University



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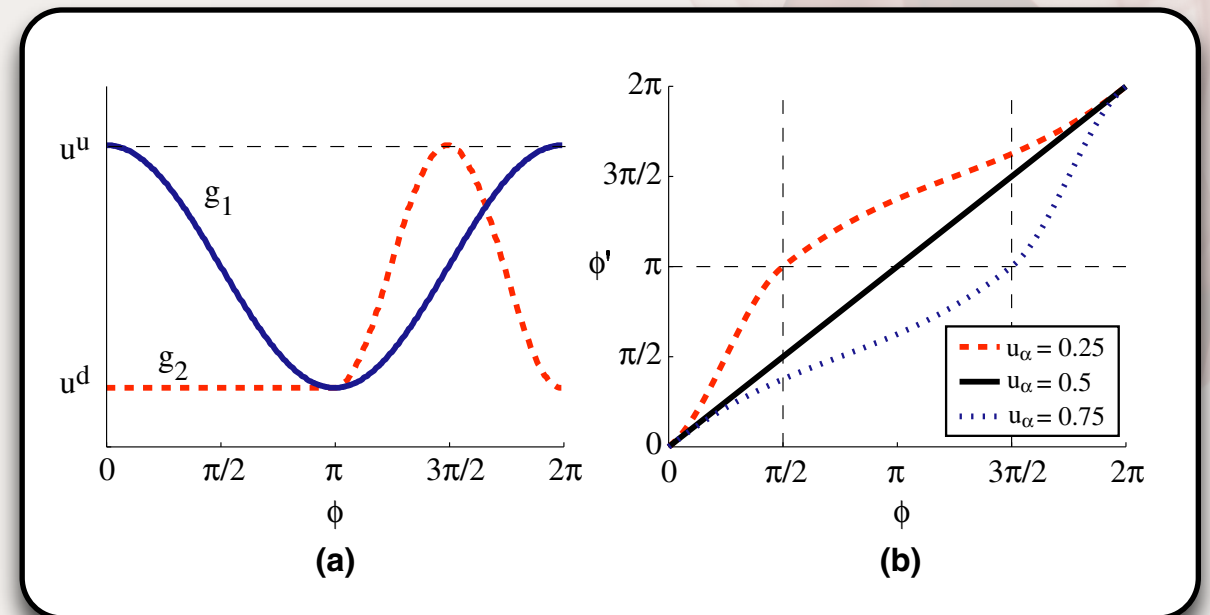
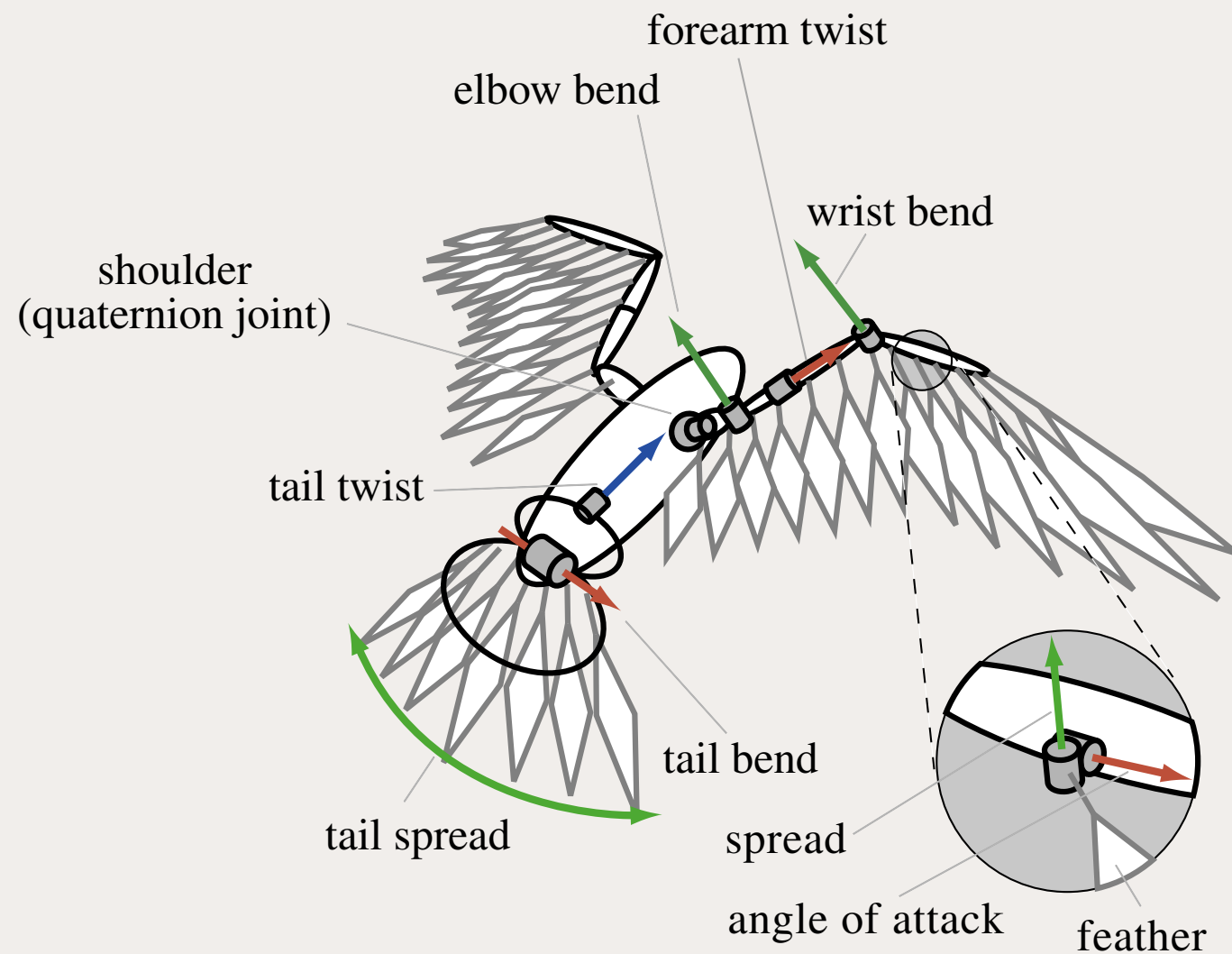


# Overview

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# Bird Flight



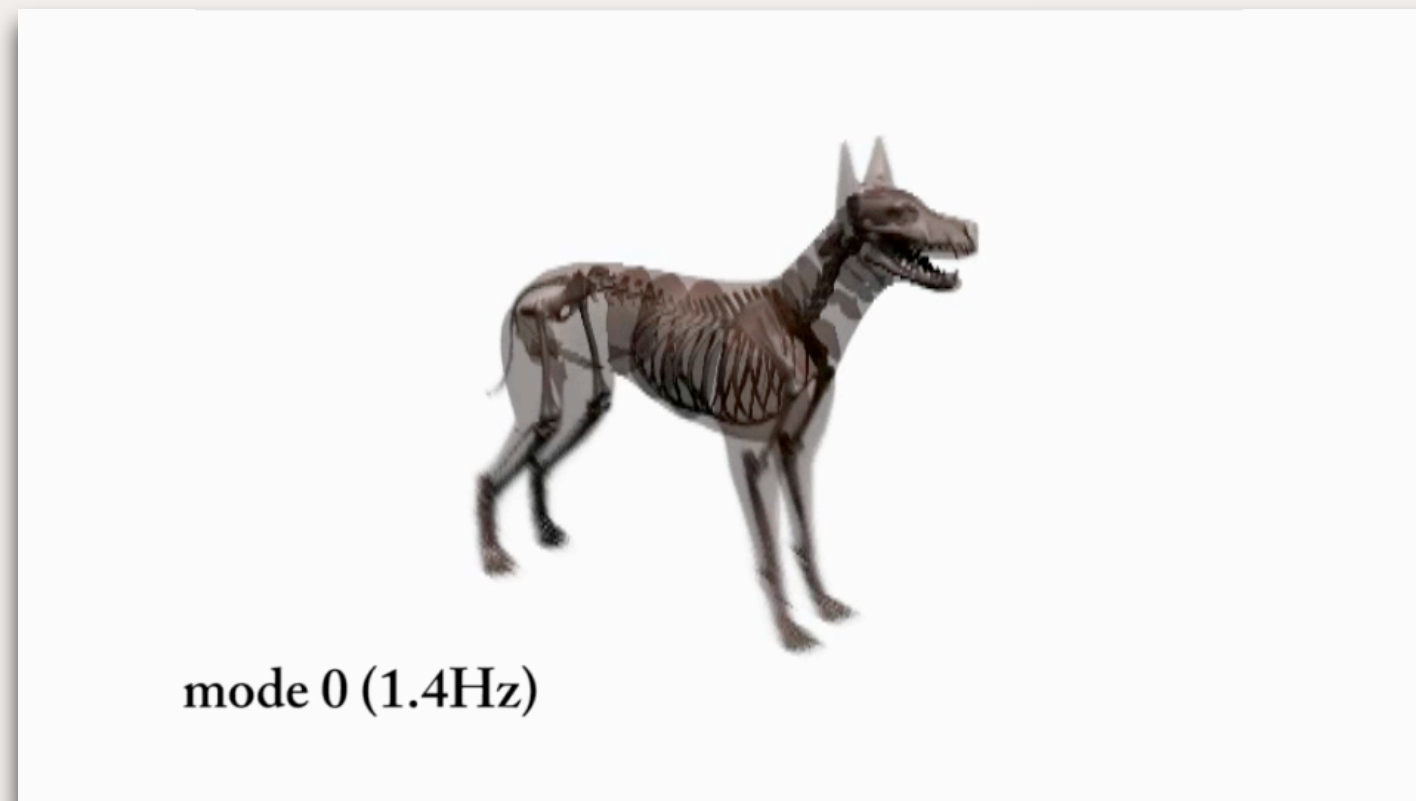
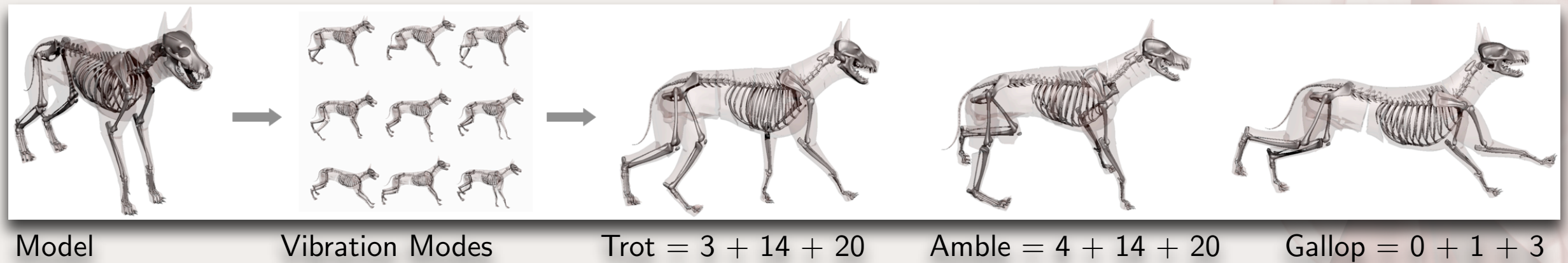
source: Wu and Popović [2003]

# Bird Flight Examples

**Eagle - Full flight path**



# Dogs



source: Kry et al [2007]

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# Overview

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# Questions



- **What might be the best physics control paradigm from the animator's perspective?**
- **How can we control physics (in general)?**
- **What about linear dynamics (like springs), vs. nonlinear dynamics (like fluids)?**
- **What about constraints? (e.g. joints)**